

COMBUSTION CHAMBER DESIGN FOR A QUENCH GASIFIER

CROSS-REFERENCE TO RELATED PATENT APPLICATIONS

This non-provisional patent application is based on a prior provisional patent application number 60/162,959 filed on November 2, 1999 by the applicant Devendra T. Barot. The following patents are cited as references in this patent application:

U.S. Patent No. 4,574,002 issued on March 4, 1986 to Barot.

U.S. Patent No. 4,828,579 issued on May 9, 1989 to Becker et al.

U.S. Patent No. 4,828,580 issued on May 9, 1989 to Dach.

U. S. Patent No. 5,464,592 issued on November 7, 1995 to Brooker et al.

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

"Not Applicable"

REFERENCE TO A MICROFICHE APPENDIX

"Not Applicable"

BACKGROUND OF THE INVENTION

U.S. Class: 48/113, 48/77, 48/74, 48/69, 48/68, 48/61, 422/207, 431/350

Quench gasifiers are used to gasify ash containing hydrocarbon feedstocks such as residual oils, waste lubrication oils, petroleum cokes and coal. A typical quench gasifier design is shown in Figure 1 (Reference: U.S. Patent No. 4,828,579). The feedstock, the oxidant and a temperature moderator (either steam or carbon dioxide) are injected into the top portion of the gasifier through a burner and are mixed with one another in the reaction zone below the burner. Steam and carbon dioxide (CO<sub>2</sub>) moderate the temperatures in the reaction zone and also act as reactants. The partial oxidation reactions that take place in this portion of the gasifier, called the combustion chamber, maintain the combustion chamber temperatures in the 2000 to 3000 °F range. The combustion chamber is lined with refractory materials such as alumina. Approximately 90.0 to 99.5 percent of the carbon in the feedstock is converted to the synthesis gases (syngas).

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The bottom portion of the quench gasifier, called the quench chamber, is separated from the combustion chamber by the floor of the combustion chamber as shown in Figure 1. The quench chamber is partially filled with water and is not lined with refractory. The quench chamber consists of three main components: the quench ring, the dip tube and the draft tube as shown in Figure 1. The main functions of the quench chamber are to cool down the synthesis gases generated in the combustion chamber by mixing them with water and to saturate the gases with water vapor.

The constricted gasifier throat area which directs the gases from the combustion chamber to the quench chamber is normally the coolest portion of the combustion chamber because of its distance from the gasifier burner and the burner flame. This area tends to be cooler than the rest of the combustion chamber also due to its proximity to the quench ring through which cooling water is injected into the quench chamber. As a result, the ash in the feedstock, which is in its molten or semi-molten form in the center portion of the combustion chamber, tends to solidify and form deposits or plugs in the throat area of the gasifier. These deposits are more likely to form with feedstocks that contain metal compounds such as vanadium trioxide ( $V_2O_3$ ) because these compounds solidify at temperatures lower than 3000 °F. In addition to causing shutdown of the gasifier, these compounds also react and damage the alumina type refractories that have been used in existing gasifiers (see U.S. Patent No. 5,464,592).

A new gasifier throat design is proposed in this invention to avoid ash deposits and plugging in the throat area of the gasifier and to avoid damage to the refractories in the throat area. The proposed design will use electrical resistor heating to achieve temperatures in the range of 3000 to 3500 °F. The new design will also use refractory materials like silicon carbide and silicon nitride that can withstand higher temperatures and larger temperature shocks than alumina. With this new design, it will be possible to increase the gasifier carbon conversion, reduce the steam (moderator) consumption and reduce the frequent damages that have been experienced to the refractories in the throat area of existing gasifiers. The proposed design will also decrease the capital cost of oil gasification plants by eliminating the need for soot recycle system downstream and will reduce the plant operating cost by improving the reliability of the gasifier operations.

#### BRIEF SUMMARY OF THE INVENTION

Electrical heating and new refractory materials are proposed for the gasifier throat area, which will increase the throat area operating temperatures without increasing oxygen consumption. The

high temperatures will improve the gasification process by increasing carbon conversion, reducing steam or CO<sub>2</sub> consumption and by eliminating ash deposits and plugging. The preferred shape for the gasifier throat with electrical heating is the wind tunnel shape proposed in the previous U.S. Patent No. 4,574,002. The gasifier throat area is heated electrically using graphite resistors to maintain temperatures in the throat area between 3000 and 3500 °F. At these temperatures, higher carbon conversion is achieved and ash deposits are melted and pushed out of the throat area by high syngas velocities achieved in the constricted throat area. The throat area refractories consist of three layers. The innermost layer or hot face that is exposed to the hot gases consists of silicon carbide or silicon nitride or a combination of the two materials. The middle layer consists of graphite resistors and the outermost layer consists of insulating refractories.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1: Prior Art Example 1, Typical Quench Gasifier Design with Conical or Funnel Shape Throat.


Figure 2: Prior Art Example 2, Typical Quench Gasifier Design with Wind Tunnel Shape Throat.

Figure 3: New Art Example, New Quench Gasifier Design with Electric Heating of the Throat Area.

Figure 4: Details of the New Throat Design

Figure 5: New Combination Quench Gasifier

#### DETAILED DESCRIPTION OF THE INVENTION



A previous patent (U.S. Patent Number 4,574,002) suggests changing the shape of the gasifier throat to avoid ash deposits and plugs in this area. The wind tunnel shape proposed in U.S. Patent No. 4,574,002 is shown in Figure 2. This shape provides a better chance of avoiding deposits and plugs in the throat area than the shape shown in Figure 1. However, the wind tunnel shape is also susceptible to deposits and plugs particularly when feedstock contains metals or metal compounds that solidify at temperatures lower than 3000 °F due to the distance of the throat from the burner and its proximity to the quench ring component of the gasifier.

In order to avoid ash deposits and plugs in the throat area, particularly with feedstocks that contain vanadium trioxide type metal compounds, it is necessary to maintain temperatures in the throat area in the 3000 to 3500 °F. At these higher temperatures, vanadium oxide type compounds (vanadium trioxide and all other metal compounds that melt and flow easily at temperatures in the 3000 to 3500 °F range) will melt and easily flow out of the throat and into the quench chamber. The throat refractory will have to withstand these high temperatures. Alumina type refractories that have been used in the throat area in the past are frequently damaged by vanadium oxide type compounds (see U.S. Patent No. 5,464,592).

This patent application proposes electrical heating (either with resistors or with electromagnetic waves) of the throat area to avoid low temperatures in the throat area. This patent application also proposes that the hot face of the throat area refractory be silicon carbide, silicon nitride or a combination of the two. As shown in Figure 4, the electrical heating elements will be made of graphite and graphite heating elements will be used behind the hot face material. The outermost layer of the throat block will be made of insulating refractory. This insulating refractory will prevent high temperature exposure of the combustion chamber floor and the quench ring.

This new design will make it possible to control temperatures in any desired range in the throat area up to an upper temperature limit of about 3500 °F. The design proposed in Figure 3 shows an approximate wind tunnel shape. The throat does not have to be exactly in the wind tunnel shape. The essential features of this design are that the ratio  $D1/D3$  be in the range of 3 to 6 and that the diameter of the throat shape should decrease as you move away from  $D1$  portion of the throat.

Figure 3 only shows an application for the electrical heating concept in the throat area of a vertical quench gasifier. In fact, this concept can also be applied to a horizontal reactor as shown in Figure 5 or to the entire hot face of the combustion chamber. This concept can also be applied to any extension of the gasifier exit area such as the transition block area of Figure 5.

Figure 5 shows a combination quench gasifier. A portion of the syngas generated in the combustion chamber is quenched in water and the remaining syngas is quenched (cooled down) by injecting a cold quench gas.